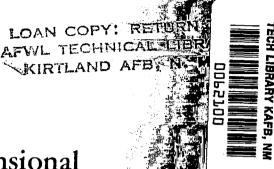
NASA Contractor Report 3221



Calculation of Two-Dimensional Inlet Flow Fields in a Supersonic Free Stream - Program Documentation and Test Cases

S. H. Biringen and O. J. McMillan

CONTRACT NAS1-15305 MARCH 1980





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S. H. Biringen and O. J. McMillan Nielsen Engineering & Research, Inc. Mountain View, California

Prepared for Langley Research Center under Contract NAS1-15305



Scientific and Technical Information Office

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1. INTRODUCTION

In this report we present listings of the source listings and a number of test cases to exemplify the use of the computer codes employed to calculate flows about 2-D inlets in a supersonic free stream and to generate computational grids. The program that calculates 2-D inlets flow fields makes use of an implicit algorithm to solve the 2-D time-dependent Euler equations (ref. 1). The mesh generation program (ref. 2) uses the algorithm developed in reference 3 to generate nonorthogonal grids.

Problem formulation, mathematical framework and the overall logic of the programs are presented in a separate report (ref. 4). In the first part of this report we present the input data, specification of initial and boundary conditions, operating instructions and answer listings obtained from the 2-D Euler solver for a drooped-cowl inlet. The test case involves supercritical inlet operation at a subdesign Mach number, M = 2.09. In the second part of this report input data, boundary conditions and answer listings are presented for the mesh generation program. Complete listings of the codes are given in Appendices A and B.

2. THE CODE FOR THE CALCULATION OF 2-D INLET FLOW FIELDS (THE EULER CODE)

In this section we present the input data, specification of initial and boundary conditions and answer listings for the drooped-cowl inlet (fig. 1) for which the design Mach number is

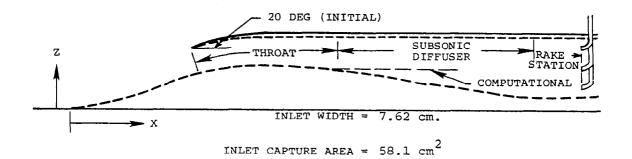


Figure 1.- Isentropic-compression, drooped-cowl inlet configuration.

 $\rm M_{\infty}=3.00$. Free stream conditions at $\rm M_{\infty}=2.09$ are prescribed as initial conditions. The incident ramp shock is captured by starting the integration downstream of the ramp leading edge and placing six points on the inflow boundary downstream of the rampleading edge shock. Values of flow variables at these locations are found from oblique shock tables (ref. 5). Initialization of flow variables is done in SUB.INITIA.

The sample input data for the 46×22 grid is given in section 2.1. The output listings from the computer program are given in section 2.2 and contour plots (obtained via a library subroutine at NASA/Ames Research Center) are presented in section 2.3.

2.1 Program Use and Operation

In this section we give a detailed description of the input information required to run a typical test case, e.g., calculation of the drooped-cowl inlet. The initial field as well as values of various constants are evaluated in SUB.INITIA. This subroutine also reads the input data except for the last card, which specifies geometry and the type of duct-outflow boundary condition to be used. This last card is read by SUB.BC. We now list the input data cards in order:

Card No.	Format		Variables
1	815	NMAX:	Maximum number of time steps
		JMAX:	Maximum number of points along ξ , where ξ is the coordinate along the body.
		KMAX:	Maximum number of points along $\eta_{\text{\tiny{$1$}}}$ where η is the coordinate that crosses $\xi_{\text{\tiny{$2$}}}$
		NP:	Incremental number of time steps after which SUB.MAP is called. The function of SUB.MAP is described in reference 4.
		METH:	Flag for upwind differencing. If METH > 0, program skips upwind differencing.
		IREAD:	Option for grid system. If READ > 0, reads grid from disc (file number 3).
		INVIS:	If INVIS > 0, program accounts for viscous effects; if INVIS = 0, the calculation is inviscid
2	715	IREGO:	If IREGO > 0, reads initial field from disc, otherwise starts from free stream conditions.
		ISTORE:	<pre>If ISTORE > 0, solution data stored on disc (file number 4).</pre>
		JTAIL1:	First ξ -interior point, set to 1.
		JTAIL2:	Last ξ -interior point, set to JMAX-1
		IPLOT:	Index for calling plot routine. If set to zero it skips the plot routine. Otherwise calls the routine at the specified interval.
3	315	IUPWIND:	<pre>If IUPWIND > 0, skips upwind dif- ferencing.</pre>
		IOSCIL:	Not relevant to this implementa- tion of this code. Set IOSCIL=0.
		LAMIN:	If LAMIN \geq 0, calculates turbulent viscosity.
4	8F10.0	· CNBR:	Courant number; set to about 10 (see ref. 4).

Card No.	Format		Variables
4		DX:	x-increment used in SUB.GRID. For grid read off the disc set DX=0.
		DY:	y-increment, as above.
		FSMACH:	Free stream Mach number.
		SMU:	Pseudo viscosity coefficient. Set to about 10 times the time step.
		EPS:	Used in SUB.GRID. Here set EPS=0.
		RE:	Reynolds number. In case of inviscid calculation set to about 10 ⁶ .
		ALPHA:	Angle of attack.
5		XOSCIL VARA VARB VARC	Not relevant to this implentation of this code. For the inlet calculation set to zero.
6	212	LFAC:	If LFAC = 1 outflow is subsonic, otherwise it is supersonic.
		JAXI:	<pre>If JAXI = 0 flow is plane 2-D, If JAXI = 1 flow is axisymmetric.</pre>

Sample Input for Test Case

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2.2 Output Listings

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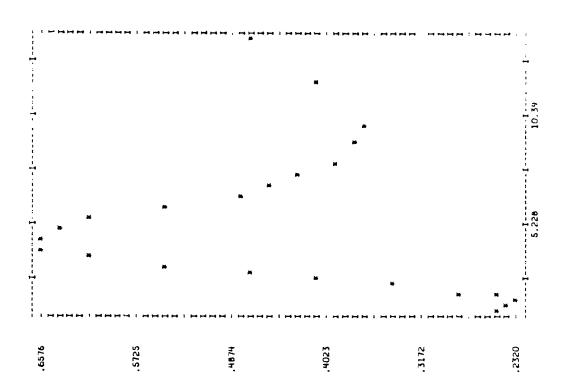
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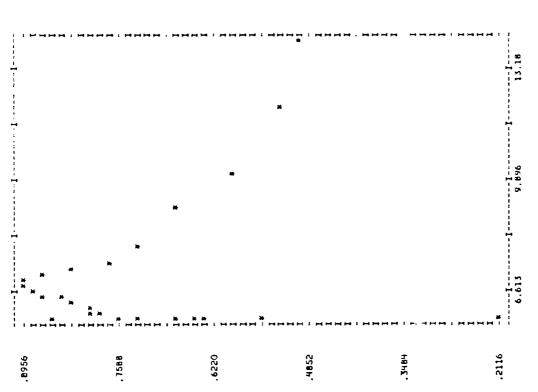
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FREE STACAM TOTAL PAGES (CT.D.) - ,8 cond (CT.)
FREE STACAM TOTAL (CS.) - ,714,4 (CO.)
FREE STACAM TOTAL (CS.) - ,714,4 (CO.)
FREE STACAM TOTAL FACTOR (CT.) - ,44 (CT.)
FREE STACAM TOTAL FACTOR (CT.) - ,44 (CT.)
FREE STACAM TOTAL FACTOR (CT.) - ,44 (CT.)
FREE STACAM TOTAL FACTOR (CT.) - ,45 (CT.)

11ER+ 0 11ML- 0.0400 DT+ .6677 HKK, TOTAL ENDALPY FRE, = 59.71% ALTERIT DAINE (P. 1. 1.25 July- 1. 1.15...) OF F. 1.14%, OTER ENTRE FILID- 3.97%, HKSC - SLANA - 0 HKSC - FLOW ALD- 1164/14/14/17 1 CHECK ON HASS FLOW ALD-C .1174/14/01 1 61 SIDDAL- .1538/917-01

6.5 2 4.	, %-551868 - 02	.2017 92 Februari	.15547606.01
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HESIDUM, 11190k-01 1970e814E-03 1426937E-02 567817. 03 HASS FLOW RAFE, M.ST 116444.031171 STEP 5 CHECK ON MASS FLOW AT J-6 112446.401 3	.36573866-62	.9118 (811 +01	.1119000E-01
RESIDUAL 1119/11-01 897253341-03 14-216541-02 56457101 05 HASS FLOW KALL, MOST 115/11/11/11/11/11/11/11/11/11/11/11/11/	30.6068 R G.	10+ 80 8016	10-316/6111
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HISTORMER - 1105GL 01 HISS FLOW ROLL, ROLL - 1164 A.+01114 S.HF 10 CHICK ON RMSS FLOW ROLL - 1164 A.+01114 S.HF 10 CHICK ON RMSS FLOW AT J-6 .11255 F.01 10	. SC# 99 GOR - O.S.	10+ Rown/ 276."	10- Resolt.
#ESTORM#	. 30 - 10 - 10 - 10 - 10 - 10 - 10 - 10 -	23 2ba 21 5-3	.110'63'E-01





R.M.S. OF TOT, ENTH, ERR. OVER ENTIRE FIELD* 3.95%. | HACH | LEAKAINF VRAKZINF | 1461F61 - 1602-1600 - 1986E-14 | 1.1451F61 - 1802-1600 0 | 1.1451F61 - 1764 F600 0 | 1.14674 - 11 - 1764 F600 0 | 1.14674 - 11 - 1764 F600 0 | 1.1555 F601 - 1764 F600 0 | 1.1555 F601 - 1765 F601 | 1.155 F601 - 1765 F601 | 1.1555 F6 IIER* 1 TIME* .0767 DT* .0077 MAX. TOTAL ENTHALPY ERR.* 58.66% AT FIRST INDEX* 28. SECOND INDEX* 1. 5751NI 1007R + 601 1007R + 61 1007 + 61 1007 + 61 174 1144 170 (101 170 (101 180 (101 187 (101 187 (101) UZQINE VZQINE BOZZE+GO 0. BOZZE+GO 0. 7987E-GO 0. 7917E-GO 0. RHO/RINF 1879E+01 1879E+01 1935E+01 20-10E+01 2159E+01 SECOND INDEX- 1 157 P/PINF 1 .2508E+01 2 .2508E+01 3 .26.1F+6-01 4 .282.1E+01 5 .3059E+01

.4931£+00 .4931£+00 .5288[+00 .5976[+00

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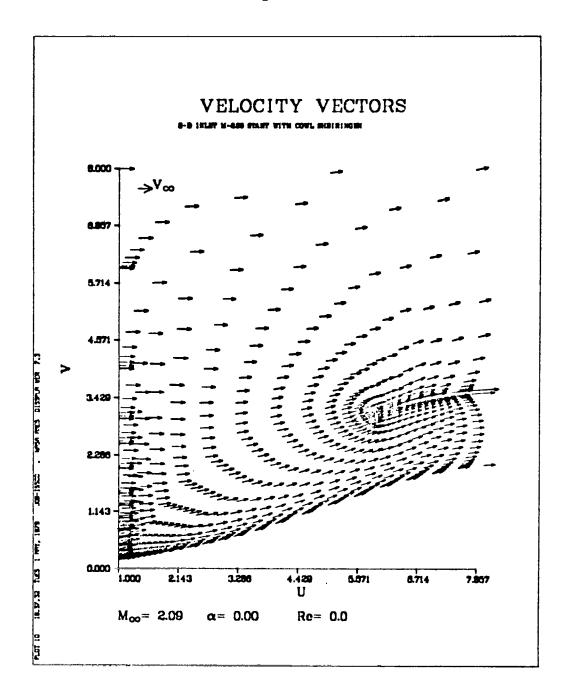
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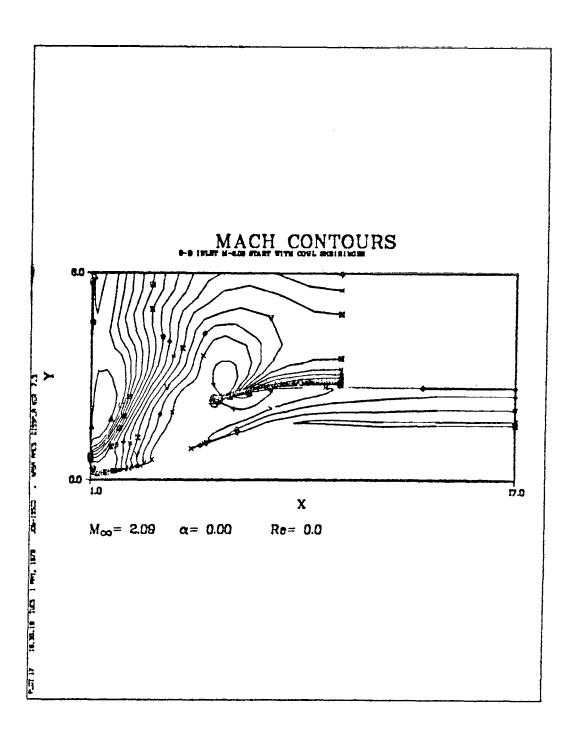
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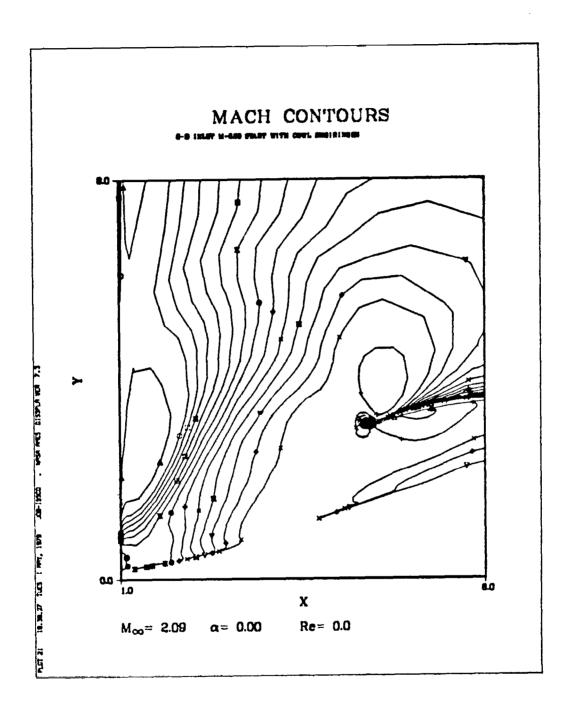
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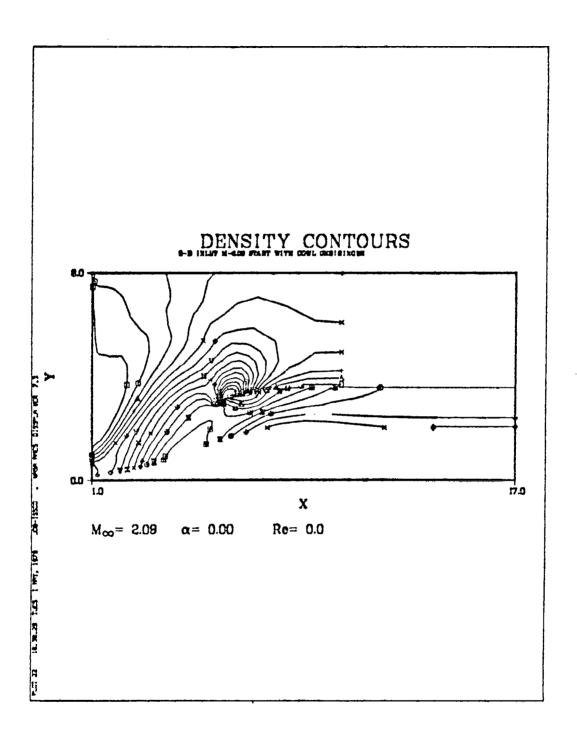
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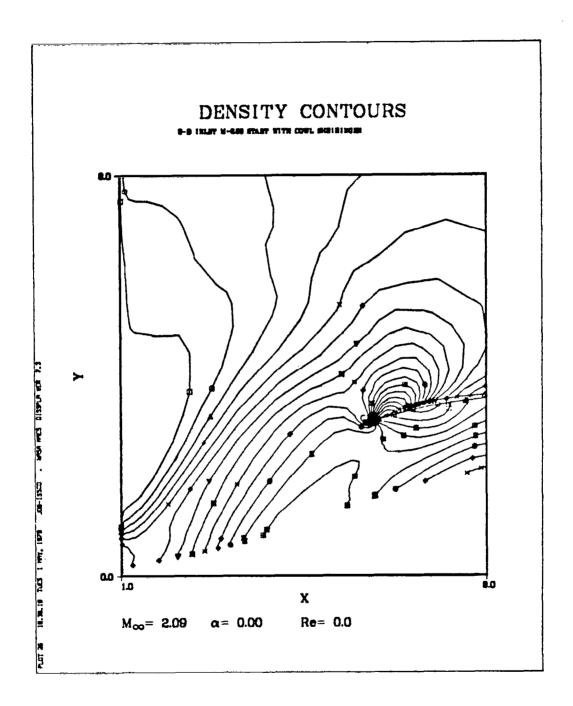
2.3 Contour Plots of Velocity, Mach Number, Density, and Pressure

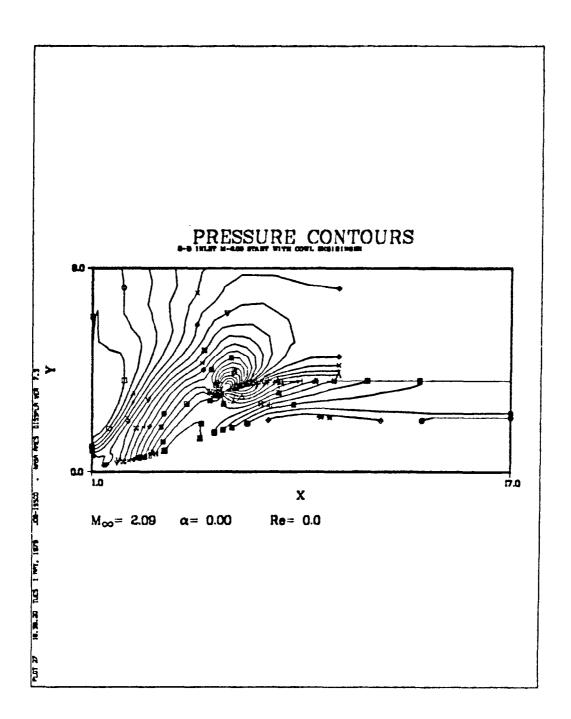


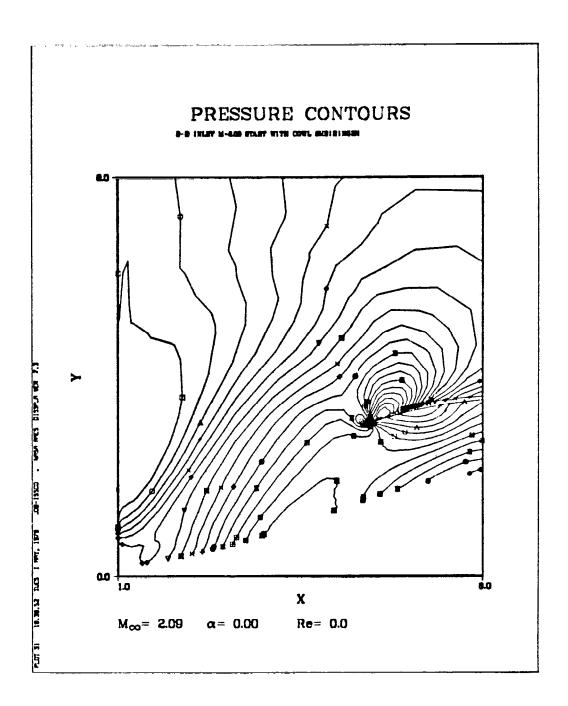












3. THE MESH GENERATION CODE

In This section we present the input data, answer listings and plots for the inlet geometry shown in figure 1. The computational grid is generated as a 46×22 mesh.

3.1 Program Use and Operation

In this section we give a description of the input information required to run a typical test case, e.g., the calculation of a nonorthogonal grid for the drooped-cowl inlet. Various subroutines have been modified to accommodate a flexibility for input data for the present calculations.

Input data is read by PROGRAM.MAIN in the following order:

Card No.	Format	Variables
1	315	JWAKE: Number of grid points in the x-direction in the wake including the trailing edge point. Set to 1 for the present calculations.
		KMAX: Number of grid points in the y-direction.
		MAXIT: Number of iterations to be used in creating the unclustered grid.
2	3F10.0	XGMX: x-direction coordinate of rear- ward boundary.
		XGMN: x-direction coordinates of front boundary.
		YMAX: y-direction coordinate of top boundary.
		YMIN: y-direction coordinate of bottom boundary.
		<pre>XNOSE: x-direction coordinate of lead- ing edge of cowl.</pre>
		XTAIL: x-direction coordinate of trail- ing edge of cowl.

Card No.	Format	Variables
		XRAMP: x-direction coordinate of lead- ing edge of ramp.
3	F10.0	DX1: Minimum y-increment on rearward boundary for initial conditions.
4	4F10.0	XORG: Location on the x-axis of the special clustering origin.
		YORG: Location on the y-axis of the special clustering origin.
		ETAC: Angle (in degrees), about which angular clustering is done.
		BETA: Parameter determining the strength of angular clustering. For equal-angular distribution set to zero. Otherwise values in the range 1 to 5.
5	F10.0	OMEGA: Parameter for Thompson solver, values between 0 to 2 recommended.
6	F10.0	DY2: Minimum y-direction spacing for final clustering.
7	A71	Title on each SC4020 plot resulting from each run.
8	A80	Description of the cowl.
9 10 54	2F10.0	Cards 9, 10, All cards following card 9 contain in columns 1 to 10 and 11 to 20 two floating-point numbers, x and y, respectively, which are coordinates of points on the cowl surface defining the airfoil shape. The points should be ordered counterclockwise.
55 • • 82	2F10.0	Cards 55, 56, Coordinates of the ramp, inflow boundary and outer boundary.

It should be noted that the number of points in the ξ -direction (along the body) is specified in PROGRAM.MAIN by assigning an integer value to the variable NBOD. We have further modified

SUB.OUTER such that it allows the boundary points along the ramp, inflow boundary and the outer boundary to be specified point by point. For each different geometry, these boundary points must be prescribed in SUB.OUTER.

Sample Input for Test Case

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3.2 Output Listings

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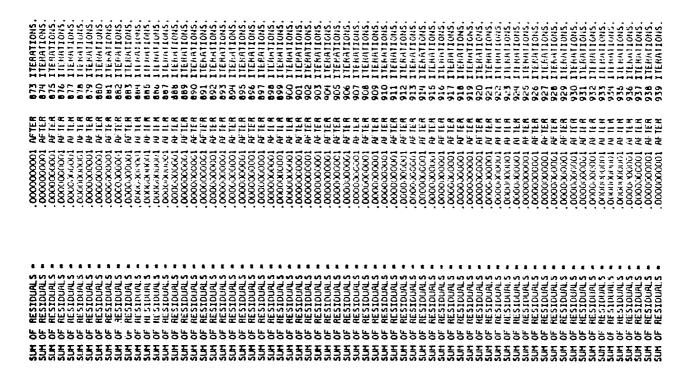
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EPSIL.	EPSIL-	EPSIL.	EP SIL .	EPSIL.	EPSIL.	EPSIL-	EPSIL.	EPSIL.	EPSIL.	EPSIL.	EPSIL.	EPSIL.	EPSIL*	EPSIL.	EPSIL.	EPSIL-	EPSIL.	EPSIL.	EPS1L.	EPSIL.	EPSIL-	EPSIL-	FPSIL.	EPSIL.	EPSIL.	EPSIL.							

			.17000E+02	.299755E+01 .207674E+01	.140420E+02 .140053E+02	.299811E+01 .207645E+01	.120081E+02	.299757E+01 .207673E+01	.101005E+02 .100135E+02	.303753E 01	.905963E+01 .900750E+01	.303857E+01 .219578E+01	.824547E+01	,300394E+01
			.170000E+02	.311718E+01 .211212E+01	.140375E+02 .140091E+02	.311800E+01	.120071E+02 .120014E+02	.311721E+01 .211211E+01	.100901E+02 .100229E+02	.314805E+01 .221781E+01	.905251E+01	.314705E+01 .222981E+01	.821891E+01	.312422E+01 .213949E+01
			.170000E+02	.322321E+01 .215829E+01	.140337E+02	.322414E+01 .215764E+01	.120058E+02	.322324E+01 .215827E+01	.100766E+02	.324613E+01 .226107E+01	.904371E+01 .901947E+01	.324376E+01 .227367E+01	.818469E+01	.322756E+01
			.170000E+02	.331342E+01 .221746E+01	.1402 <i>5</i> 4£+02 .140192£+02	.331434E+01 .221666E+01	.120045E+02	.331345E+01 .221744E+01	.100418E+02	.332974E+01 .231627E+01	.903451E+01	.332671E+01 .232923E+01	.814762E+01	.331219E+01 .222873E+01
ons.	ONS.		.170000E+02	.338754E+01 .229158E+01	.140193E+02 .140253E+02	.338835E+01 .229067E+01	.120033E+02	.339756E+01 .229156E+01	.100473E+02 .100622E+C2	. 339863E+01 . 238516E+01	.902586E+01 .903617E+01	.339555E+01 .239804E+01	.811171E+01 .#14613E+01	.337874E+01 .229531E+01
T 3 ITERATIONS	R 3 ITERATIONS		.170000E+02	.344671E+01 .238179E+01	.140138E+02	,344736E+01	.120023E+02 .120057E+02	.344673E+01 ,238176E+01	.100341E+02 .100769E+02	.345385E+01 .246877E+01	.901828E+01	.345114E+01 .248099E+01	.807957E+01	.342957E+01 .237983E+01
00000 AFTER	DOO AFTER		.170000E+02	.349288E+01 .248782E+01	.140091E+02 .140375E+02	.349335E+01 .248701E+01	.120015E+02	.349289E+01 .248779E+01	.100228E+02 .100904E+02	.349714E+01 .256685E+01	.901200E+01	.349505E+01 .257772E+01	.805243E+01 .821791E+01	.346767E+01 .248311E+01
F	. F00000		17000E+02 .170000E+02	F J* 1 .352826E+01 .260745E+01	.140053E+02 .140420E+02	.352855E+01 .260690E+01	T J* 3 .120009E+02 .120080E+02	,352827E+01 .260744E+01	,100134E+02	,353050E+01 .267739E+01	. 900696E+01 . 906064E+01	.352914E+01 .268623E+01	. 803018E+01	.349574E+01 .260329E+01
ONB 87800.	00956 AND	CLUSTERING	XI LINE A' 2000E+02 2000E+02 2000E+02	.355500E+01 .355500E+01 .273638E+01 .203000E+01	.140023E+02 .14044SE+02 .14044SE+02	NT XI LINE A. .355513E+01 .273618E+01 .203000E+01	1000 M	TANT X1 LINE AT .355500E+01 .273638E+01 .2030G0E+01	(I LINE R) 3059E+02 1064E+02 3000E+02	.355508E+01 .355508E+01 .279643E+01 .214000E+01	CONSTANT XI LINE AT 0E+01 . 9003035+01 0E+01 . 900416E+01 BE+01 . 900000E+01	7002 8	A 1200	KI LINE A1 1635E+01 5538E+01 7500E+01
EPSIL- 1.0	EPSIL- 1.(AFTER FINAL C	x 5 FOR CONSTANT) .170000E+02 .170.000E+02 .170.000E+02 .170.000E+02 .170.00E+02 .170.00E+	Y 5 FOR CONSTANT XI .357500E+01 .35550 .28686ZE+01 .27363 .205000E+01 .20300	X S FOR CONSTRNT) .1400006+02 .141 .140445E+02 .141	Y S FOR CONSTR ,357500E+01 ,286882E+01 ,204987E-01	X S FOR CONSTANT XI LIN .1200006.02 .1200046 .1200866.02 .1200066.	Y S FOR CONSTR .357500E+01 .296863E+01 .205000E+01	x s FDR CONSTANT > 100000E+02 .100 .101063E+02 .100 .100059E+02 .100	Y 5 FOR CONSTRNT XI LIN 1357500E+01 .35550BE+ 291849E+01 .279643E+ 215911E+01 .214000E+	X S FOR CONSTI .900000E+01 .906380E+01	Y S FOR CONSTANT XI LIN .357500E+01 .355523E+ .26220E+01 .280274E+ .216973E+01 .215000E+	X 5 FOR CONSTRNT XI LIN .800000E+01 .801324E+ .82599E+01 .825979E+ .801297E+01 .800000L+	Y S FOR CONSTRNT) .353140E+01 .353 .289180E+01 .273

.777876E+01	.295301E+01 .204743E+01	.747261E+01 .703672E+01	.193494E+01	.721873E+01 .654070E+01	.272024E+01 .180026E+01	.697664E+01 .604216E+01	.260292E+01 .165483E+01	.673947E+01 .554165E+01	.248661E+01 .147477E+01	.649907E+01 .504156E+01	.237800E+01	.625450E+01 .454139E+01	.227943E+01
.775038E+01 .754929E+01	.307587E+01 .207658E+01	.746071E+01 .706446E+01	.290400E+01	.723419E+01 .657272E+01	.287704E+01	.702552E+01 .607666E+01	.278223E+01	.682345E+01 .557698E+01	.268906E+01	.662523E+01 .507788E+01	.260014E+01	.642916E+01 .457851E+01	.251521E+01
.771179E+01	.318020E+01	.743415E+01 .710023E+01	.310164E+01	.722922E+01	.301337E+01 .185016E+01	.704352E+01 .612415E+01	.293938E+01	.686674E+01 .562700C+01	.286810E+01	.669585E+01 .513046E+01	.279960E+01	.653037E+01 .463332E+01	.273256E+01
.766918E+01	.326417E+01 .216716E+01	.740002E+01 .714504E+01	.319674E+01 .203794E+01	.721240E+01 .667114E+01	.312476E+01 .189051E+01	.704356E+01	.306764E+01 .174224E+01	.688364E+01	.301364E+01	.672941E+01 .520531E+01	.296152E+01	.658061E+01	.290992E+01
.762772E+01 .764630E+01	.332008E+01	.736454E+01 .719893E+01	.327023E+01 .209931E+01	.71°140E+01 .674144E+01	.321170E+01 .194568E+01	.703538E+01	.316707F+01	.608708E+01	.312513E+01 .163137E+01	.674335E+01 .630926E+01	.308415F+01 .146606E+01	.660375E+01	.304308E+01
.759070E+01 .768776E+01	.337726E+01 .231852E+01	.733180E+01 .726001E+01	.332517E+01 .217987E+01	.717125E+01 .682644E+01	.327752E+01 .201972E+01	.02526E+01	.324151E+01	.688520E+01 .591410E+01	.320723E+01	.674845E+01 .544888E+01	.317301E+01 .155481E+01	.661447E+01 .498086E+01	.313814E+01
.755956E+01 .772&77E+01	.3412796+0. .2421966+01	.730385E+01 .732413E+01	.336539E+01 .228202E+01	.716441E+01 .692169E+01	.332640E+01 .211745E+01	.701622E+01 .650539E+01	.329594E+01 .196227E+01	.688204E+01 .606852E+01	.326611E+01 .181114E+01	.675003E+01 .562807E+01	.323560E+01	.661974E+01 .518406E+01	.320397E+01
753453E+01 .753453E+01 .776364E+01	J= 7 .343847£+01 .254316E+01	.728119E+01 .738472E+01	.339430E+01 ,240569E+01	9.714146E+01 .701928E+01	. 336227£+01 .336227£+01 .2241235+01	. 700908E+01 .664427E+01	.333511E+01 .208517E+01	.687907E+01 .624864E+01	.330760E+01 .193630E+01	, 675032E+01 .584521E+01	.327886E+01	.662252E+01 .643510E+01	13 .324870E+01
7NT XI LINE AT .751496E+01 .778612E+01 .750000E+01	.345702E+01 .26775F+01 .267757E+01	TANT XI LINE AT . 726349E+01 . 743376E+01 . 700000E+01	TANT XI LINE AT .341505E+01 .254693E+01 .190500E+01	TANT XI LINE AT .713195E+01 .710798E+01 .650000E+01	CONSTANT XI LINE AT E+01 .338834E+01 E+01 .238910E+01 E+01 .177500E+01	. 700383E+01 . 700383E+01 . 678036E+01 . 600000E+01	ANT XI LINE A1 .336297E+01 .223822E+01 .163100E+01	.687675E+01 .687675E+01 .643565E+01 .55000CE+01	.333647E+01 .20929CE+01 .144900E+01	.675022E+01 .675022E+01 .608293E+01 .500000E+01	ANT XI LINE A1 .330840E+01 .196567E+01 .126690E+01	TANT XI LINE AT .662409E+01 .572056E+01 .450000E+01	ANT XI LINE AT .327872E+01
x s FOR CONSTI .750000E+01 .779158E+01 .751222E+01	Y S FOR CONST. 347040E+01 281735E+01 202585E+01	X 5 FOR CONST. .725000E+01 .746418E+01 .701569E+01	Y S FOR CONST. 342990E+01 .269762E+01 .191752E+01	x S FOR CONSTR .712500E+01 .717671E+01	Y S FOR CONST .340710E+01 .255364E+01 .178547E+01	x s FOR CONSTA .700000E+01 .689604E+01 .601748E+01	Y S FOR CONST .338260E+01 .241560E+01 .164080E+01	x s FOR CONSTR .687500E+01 .660769E+01 .551702E+01	Y S FOR CONSTR .335640E+01 .228061E+01 .145951E+01	x s FOR CONST .675000E+01 .631208E+01 .501677E+01	Y \$ FOR CONST .332840E+01 .215922E+01 .127775E+01	\$ 5 FOR CONST .662500E+01 .600762E+01 .451653E+01	Y S FOR CONSTRNT .329870E+01 .3

.111321E+01	.600232E+01 .404122E+01	.219508E+01	.576666E+01 .364044E+01	.214733E+01 .793484E+00	,552883E+01 ,324040E+01	.2116325.01 .671444E+00	.531664E+01 ,29396BE+01	.211605E+01 .592726E+00	.511449E+01 .263932E+01	.213169E+01	.491868E+01 .233922E+01	.216004E+01 .450454E+00	.473418E+01 .203944E+01
.113837E+01	.623198E+01	.243583E+01	.604306E+01 .367812E+01	.238066E+01 .822187E+00	.327853E+01	.233853E+01 .701066E+00	.\$66911E+01 .297743E+01	.232394E÷01 .623783E÷00	.\$49601E+01	.232991E+01 .551112E+00	.532767E+01	,235191E+01 ,483150E+00	.517009E+01 .207791E+01
.117527E+01	.636971E+01 .413582E+01	.266616E+01	.621728E+01	.261140E+01 .865345E+00	.606549E+01	.25610SE+01 .746067E+00	.591855E+01 .303875E+01	.252895E+01	.\$7770SE+01	.251684E+01 .600373E+00	.563763E+01 .243654E+01	.252098E+01	.\$50622E+01 .213845E+01
,122836E+01	.643809E+01	.285760E+01	.630479E+01	.928940E+01	.617899E+01	.276089E+01	.606055E+01	.271999E+01 .742247E+00	.594914E+01	.269436E+01 .674631E+00	.583938E+01	.268033E+01	.573437E+01 .223237E+01
.130266E+01	.646911E+01 .434113E+01	.300092E+01	.634213E+01 .394654E+01	.295985E+01	.622530E+01 .355638E+01	.291653E+01 .909983E+00	.812126E+01 .325687E+01	.287563E+C1 .845443E+00	.603017E+01	.204634E+01	.594554E+01 .266632E+01	. 724035E+00	.586584E+01
.140266E+01	.648372E+01	.310193E+01	.635795E+01 ,412436E+01	.306518E+01	.524051E+01	.302620E+01	.613746E+01	.298769E+01 ,988951E+00	.605312E+01	.295991E+01 .935447E+00	.598412E+01	.293522E+01 .864167E+00	.\$92352E+01 .258466E+01
.153044E+01	.649134E+01 .473716E+01	.317091E+01	.636574E+01 .436515E+01	.313627E+01 .130556E+01	.624536E+01	.309965E+01	.613636E+01	.306256E+01	. 604770E+01	,303592E+01	. \$10039E+01	, 301264E • 01 , 100688E • 01	.593577E+01 .287853E+01
.16BJZZE+01	.502147E+01	7 J- 14 .321685£+01 .157066E+01	.637027E+01	.318328E+01	1 J- 16 .624749E+01 .432843E+01	.314773E+01 .143075E+01	.405145E+01	.311100E+01 .140334E+01	. 378237E+01	137906E+01	. 597340E+01 . 351904E+01	. 304094E+01 .135724E+01	7 J= 20 .592717E+01 .326399E+01
.18566BE+01	TANT XI LINE AT 649836E+01 \$35176E+01 400000E+01	TANT XI LINE AT . 324727E+01 . 176254E+01 . 902900E+00	TANT XI LINE AT .637317E+01 .503222E+01 .360000E:01	NT XI LINE A. .321398E+01 .170861E+01 .762400E+00	ANT XI LINE AT 624901E+01 471742E+01 320000E+01	ANT XI LINE AT .317882E+01.166273E+01.6539800E+00	ANT XI LINE AT .612771E+01 .445737E+01 .290000E+01	KI LINE A' 4208E+01 5121E+01 9800E+00	NT XI LINE A. .601411E+01 .420636E+01 .260000E+01		. \$56028E+01 . \$56198E+01 . \$54198E+01 . 23000CE+01	.308980X.01 .16453:N:01 .16460E+00	ANT XI LINE AT 591293E+01 372774E+01 200000E+01
.205495E+01	X S FOR CONSTI .650000E+01 .569405E+01 .401630E+01	Y S FOR CONSTR .326720E+01 .196997E+01 .914543E+60	X S FOR CONST .637500E+01 .541327E+01 .361590E+01	Y S FOR CONSTA .323390E+01 .192534E+01 .774650E+00	X \$ FOR CONSTR .625000E+01 .513414E+01 .321579E+01	Y S FOR CONSTANT 319080E+01 .31 .169403E+01 .16.652198E+00 .63	X S FOR CONSTR .612500E+01 .489577E+01 .291545E+01	Y S FOR CONSTRNT 316190E+01 .3109410E+01 .164.572658E+00 .552658E+00 .552658E+00 .552658E+00 .552658E+00 .555	X S FOR CONSTR .60C230E+01 .466717E+01 .261526E+01	Y S FOR CONSTANT XI LINE .312310E+01 .310831E+0 .190539E+01 .164615E+0 .498501E+00 .485400E+0	X S FOR CONSTR .595000E+01 .444517E+01 .231516E+01	Y S FOR CONSTR ,310710E+01 ,192477E+01 ,42959E+00	x s FOR CONSTA .\$90000E+01 .423410E+01 .201519E+01

.220140E+01 .391944E+00	.458028E+01 .183843E+01	.22633E+01 .35444BE+00	.443550E+01	.233528E+01 .318554E+00	.432301E+01 .153569E+01	.242688E+01 .303229E+00	.421835E+01	.252744E+01 .287551E+00	.412174E+01 .133209E+01	.263736E+01	.403658E+01 .123046E+01	.255334E+00
.239065E+01 .424937E+00	.503436E+01 .187615E+01	.244831E+01 .388977E+00	.490874E+01 .167493E+01	.251810E+01 .354274E+00	.480846E+01	.260407£+01 .341279£+00	.471793E+01 .146753E+01	.269990E+01	.463754E+01 .136423E+01	.280562E+01	.457160E+01 .126116E+01	.298880E+01
.254423E+01 .476394E+00	.193576E+01	.258625E+01 .443028E+00	.828052E+01	.264219E+01 .410440E+00	.819173E+01 .162748E+01	.271320E+01 .461207E+00	.511329E+01	.279467E+01 .390925E+00	.504590E+01	.288603E+01	.499443E+01	.298720E+01 .368162E+00
.268380E+01	.663611E+01 .202871E+01	.270407E+01 .526063E+00	.554487E+01	.273919E+01 .497125E+00	.546701E+01	.278957E+01 .493817E+00	.539845E+01 .160678E+01	.285111E+01 .488974E+00	.534024E+01	.292281E+01 .482938E+00	.529770E+01	.300380E+01
.281208E+01	.\$78881E+01	.841297E+01	.571536E+01	.627121E+00	.564972E+01	.285544£+01 .633786E+00	.55905/E+01	.289525E+01 .636428E+00	.653936E+01	.294580E+01 .638613E+00	.650211E+01	.300600E+01 .640153E+00
.291926E+01 .839399E+00	.238061E+01	.290903E+01 .827154E+00	.581208E+01	.290779E+01 .813841E+00	.876072E+01	.291768E+01 .832310E+00	.871225E+01	.293752E+01	.566810E+01	.296793E+01 .863195E+00	.563478E+01	.300882E+01
.299716E+01 .106357E+01	, 889405E+01	.298403E+01	.585564E+01	.297582E+01	.236295E+01	.297434E+01 .110110E+01	.578318E+01	.297908E+01	.210677E+01	.299224E+01	.571856E+01	.301606E+01
7 J= 20 .304675E+01 .134085E+01	7 J- 21 .589385E+01 .306835E+01	.303464E+01 .135975E+01	7 J= 22 .586697E+01 .287910E+01	.30266E+01	7 J- 23 .584219E+01	7 J* 23 .302026E+01 .143326E+01	.681786E+01 .262069E+01	.301725€+01 .148732€+01	. 579268E+01 . 249702E+01	.301797E÷01 .154217E÷01	7 J- 26 .576983E+01 .237764E+01	7 J* 26 .302734E+01 .159981E+01
ANT XI LINE AT .307511E+01 .165085E+01 .357900E+00	18NT XI LINE AT . 588349E+01 . 354247E+01 . 180000E+01	FANT XI LINE AT .306477E+01 .168817E+01 .319000E+00	.586409E+01 .336441E+01 .356441E+01	7ANT XI LINE AT ,305763E+01 ,172865E+01 ,282100E+00	TANT XI LINE AT	TANT XI LINE AT .305214E+01 .18017SE+01 .264500E+00	.582923E+01 .310850E+01 .140000E+01	1304736E+01 187771E+01 246900E+00	ANT XI LINE AT .581292E+01 .298737E+01 .130000E+01	7ANT XI LINE AT 304298E+01 195745E+01 .229200E+00	.579618E+01 .287208E+01 .120000E+01	ANT XI LINE AT .304273E+01 .204324E+01 .211600E+00
V S FOR CONSTI .309080E+01 .195351E+01 .3710H2E+00	X S FOR CONSTR .587200E+01 .406308E+01	Y S FOR CONSTI .308150E+01 .200715E+01 .332653E+00	X 5 FOR CONSTA .585800E+01 .389976E+01 .161445E+01	Y S FOR CONSTR .307680E+01 .206805E+01 .296104E+00	x s FOR CONSTR .584400E+01 .377638E+01 .151366E+01	Y S FOR CONSTR .307210E+01 .215463E+01 .279360E+00	x s FOR CONSTANT .583000C+01 .5 .36585E+01 .3 .141292E+01 .1	Y \$ FOR CONST. .306740E+01 .224809E+01 .262473E+00	x s FOR CONST .581600E+01 .354663E+01 .131223E+01	Y S FOR CONST .306270E+01 .234892E+01 .245373E+00	X 5 FOR CONST. .580800E+01 .344265E+01	Y S FOR CONST. .305990E+01 .245935E+01 .228282E+00

X S FOR CONSTANT XI LINE AT J- 27

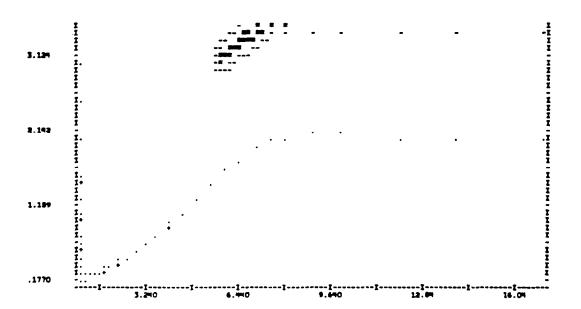
			_								
. 386285.01 . 112894E-01	.289124E+01	. 102752E+01	. 223118E+00	. 102527E+01	25 76 74E-00	. 992414K-01 . 102334E+01	. 396940E -01	. 102090E+01	. \$4054K-01	. 10190 NE +01	.82187K+01
.461993E+01	. 201934E-01		. 118764F-01	.480778E-01	. N'8940E+01	.481978E-01	. ************************************	.441122E+01	. 344261E+01 . 841818E+00	.46996#E-01	. 362673E+01
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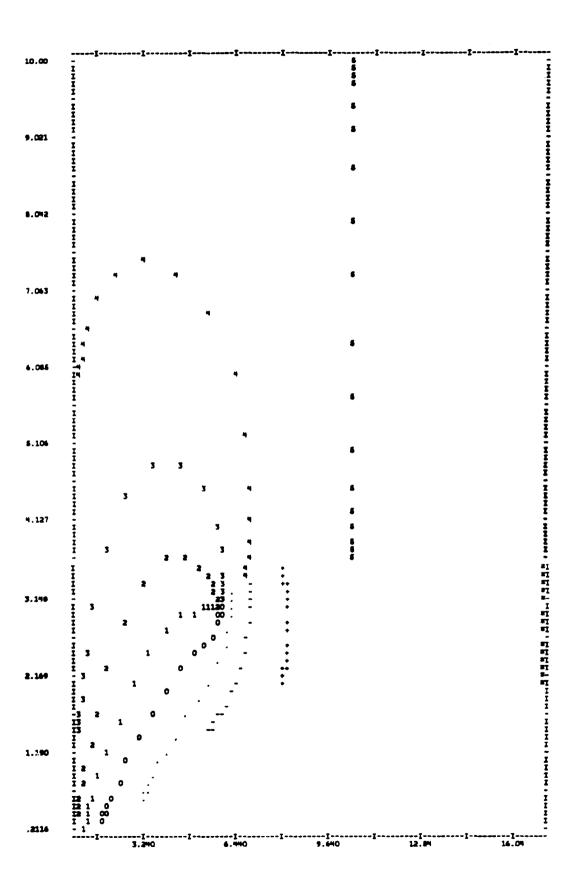
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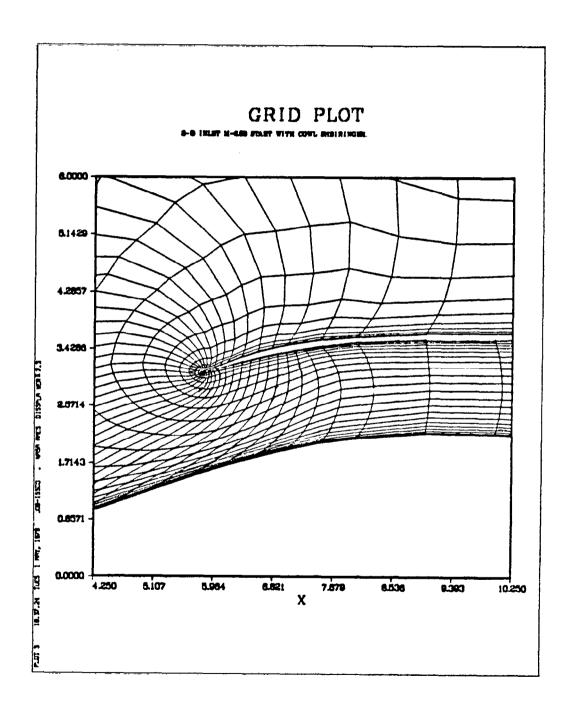
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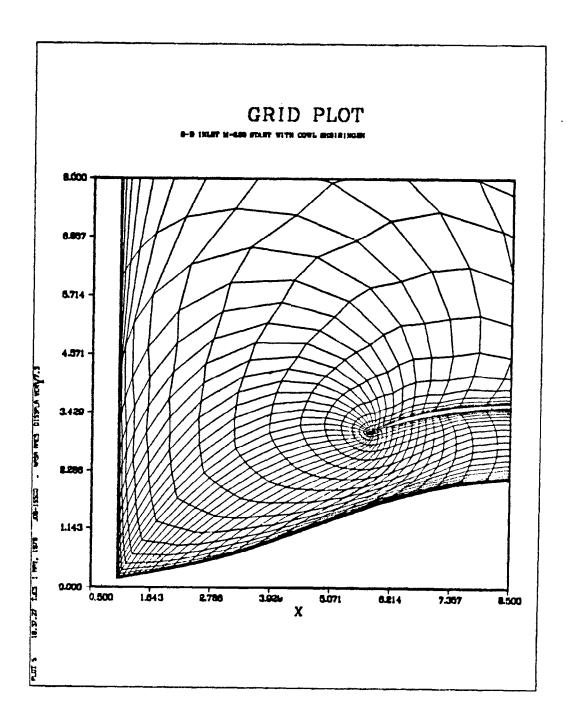


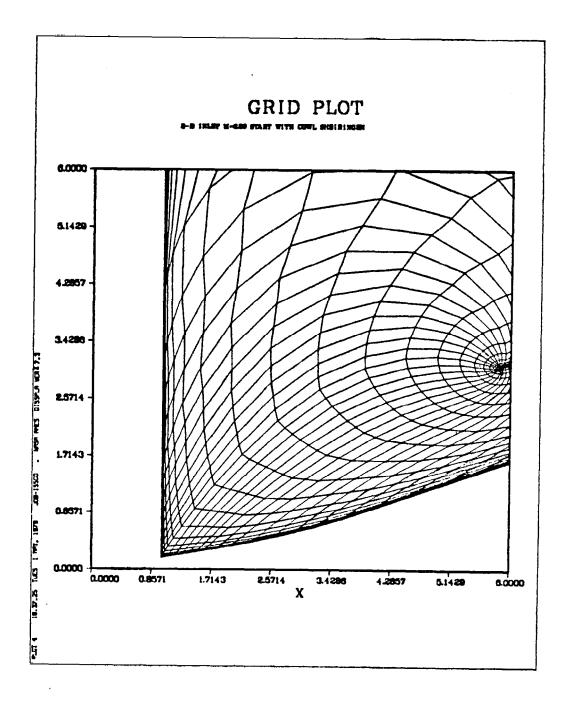




3.3 Plots of the Generated Mesh







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APPENDIX A

SOURCE LISTING OF THE 2-D INLET CALCULATION PROGRAM

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01/09/80	XYMETS INLET BASE BASE	BASE BASE VARS VARS	VARS INLET INLET INLET XYMETS	XYMETS XYMETS XYMETS XYMETS	XYMETS XYMETS XYMETS XYMETS	XYHETS XYHETS XYHETS	XYMETS XYMETS XYMETS XYMETS	XYHETS XYHETS XYHETS XYHETS	XYHETS XYHETS XYHETS B INLET	AXYHETS XYHETS XYHETS XYHETS XYHETS	XYMETS NUCT NUCT XYMETS XYMETS XYMETS	NET
FTN 4 6-460	JH, KH, DT, FSHACH, EPS, GAMHA, GAMI, SMU, HO. P. METH, ALPHA, INVIS, IPLOT, RESID	TAIL1, JTAIL2, 105C1L, XOSC1L, 1UPSNAD RC 88 36, 41, P178–361 361, S178, 36, 41, X11178, 361, ETT178, 361	HE METRIC COEFFICIENTS ACCORDING TO COBIAN	VVO 10 J-Z-JF XY(J,K, 4) = (X(J-1,K) - X(J-1,K)) = 5 10 XY(J,K, 3) = (Y(J-1,K) - Y(J-1,K)) = 5 XY(I,K, 4) = 5 = (-3 = X(1,K) -4 = X(2,K) - X(3,K)) XY(I,K, 3) = 5 = (-3 = Y(1,K) +4 = X(2,K) - X(3,K) +4 =	1 -4 *Y(UH,K) - Y(UH-1,K)) * 5	J.K-1)1* 5 J.K-1)1* 5 *X(J.Z) - X(J.31)* 5 *Y(J.Z) - Y(J.31)* 5 *Y(J.Z) - Y(J.31)* 5	XYTJ.KHAX. II = (3 *TIJ.KHAX) -4 *TIJ.KH) • TIJ.KH-III • 5 21 CONTINUE A SPATIALLY AVERAGED JACOBIAN IS NECESSARY FOR THE ACCURATE FLOW D 30 JI.JHAX D - 1 - 1	ل • RL • PL	FF (K EQ 1 OR K EQ KHAX) KP + KR + K DINV + 4 / ((XYL) KP 4) + XYLJ KR,41)+ (XYLJ K, 11+XYLJR,K,11) 1 - (XYLJ,KP,31+XYLJ,KR,31)+ (XYLJP,K,2)+ XYLJR,K,21) THIS IS A NOW SPATIALY AVERAGED JACOBIAN SINCE SOLUTION IS TO A STEADY STATE ANSWER)-XY(J,K,2)*XY(J,K,3))	/Dx. xY2*DX1/DY. V	
OPT=2 TRACE	YYMETS 'NTIME 'VMAX, JMAX, KMAX, '4), RE, P1, Z(80), N	1, ISTORE, NF, NB, J IIM, VARA, VARB, VA (0178, 36, 4), XYI (7/178, 36), Y176,	S.XIT.ETT NE CALCULATES T EM FORMS THE JA Y3-DY/DXI	5*(-3 *X(1,K) - X(1,K) - X(1,	* (3 *YC)HAX,K XY1*DY/DETA AX	(X(J,K+1) - X(Y(J,K+1) - Y(-3 *Y(J,1) *A (-3 *Y(J,1) *A (-3 *Y(J,1) *A	* (3 *YIJ,KMA ERAGED JACOBIAN	מא ט בים טא אא	OR K EG KH (XYL) KP.4) • X P.3) • XYL) KR.3 ON SPATIALLY AV	J.K.41*XY(J.K.1 V AX AX	DINV = P(J,K) Y(J,K) S THE JACOBIAN XYI=DXI/DX, XY3-DETA/DY XY(J,K,1) = XY(J,K,1)=DINV XY(J,K,2) = -XY(J,K,2)=DINV XY(J,K,3) = -XY(J,K,3)=DINV 32 XY(J,K,4) = XY(J,K,4)=DINV	1160 T0 63
76/76	SUBROUTINE XYMET COMMON/ZAM/NTIME COMMON/BASE/NMAX FV14), FD14), RE	CNBR TREGO LAMIN SMU MON/VARS/ MON/LARGE	EL 2 x. Y. S. SUBROUT! CRID SYST DX/DXI X	0.000 0.000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000	1044X K.33 411NUE 60X70E1A 201 U+1 UH	10.00 10.00	1) KHAX 13 4T1NUE 1T1NUE 30 J*1, JH	LF(J EQ 1 G D0 30 K*1, KMAX KP * K * 1	K EQ 1 4V * 4 /(1 XY1J,K 41S 1S A N 1 STEADY S	1 K) * DIN 1 K) * DIN 1 TINUE 32 J=1. JM 32 K=1. KH	10 THE UA 10 THE UA 10 TA/DX A 10 TA/DX	NTIME GT.
SUBROUTINE XYMETS		`	000 **********************************	2	2 2 2	8	Ç X 0 7 7 7 8	54 <u>-</u> 874		<u>₹</u> 2568	2	<u>i</u>
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SHOOTH 2 BASE 3 BASE 3 BASE 4 VARS 5 VARS 5		INLET 131 INLET 132 SHOOTH 9 SKOOTH 10 SKOOTH 11	SMCOTH 13 SMCOTH 14 SMCOTH 15 SMCOTH 16			SMOOTH 27 SMOOTH 28 SMOOTH 29 SMOOTH 30 SMOOTH 31		SMOOTH 37 SMOOTH 38 SMOOTH 39 SMOOTH 40 SMOOTH 40	SHOOTH 43 SHOOTH 45 SHOOTH 45 SHOOTH 47 SHOOTH 48 SHOOTH 49 SHOOTH 50
SUBROUTINE SHOOTH COTHON/BASE/MHAX, JH KM, DT, FSHACH, EPS, GAMMA, GAMI, SMU, HD, 1 FV(14), FD(14), FE, PI, 2 (801, NP, HETH, ALPHA, INVIS., IPL0T, RESID 2. CNBT, IREGO, ISTGRE, NF, NB, JTAILL, JTAILLZ, IOSCIL, XOSCIL, IUPWND 3. 'LAHIN, SHUIH, VARB, VARB, VARC COMHON/VARS/ Q178, 36, 41, X1(78, 36, 41, P178, 36) COMHON/LARGE/X178, 36, 17(78, 36, 15), X17(78, 36), ETT178, 36)		ADJACENT TO BOUNDARIES SECOND SECOND ORDER SHOOTHING DOED EXPLICITLY WITH 0 5 OF SMU HORDER SHOOTHING, ADDED EXPLICITLY TO RHS TORDER AT FRINGES WITH 5 OF SMU ** JH -1 ** JH -1 ** KH-1	SDT * SHU*DT C XI DIRECTION SHOOTHING DO 40 K=2.KH IFI IUPWING GT 0 1 GO TO 49	RINV = 1 /010,K 1) U = XIT(J,K + RINV*(XY(J,K, 1)*Q(J,K, 2) + XY(J,K, 2)*Q(J,K, 3) PP= GAM!*(Q(J,K, 4) + S*(Q(J,K, 2)**2+Q(J,K, 3)**2)*RINV C = SQRT! GAMA*PP*(XY(J,K, 1)**2*XY(J,K, 2)**2)*RINV IMC + 1 - CC	UPC * U • CC UPC * U • CC EF(J) * 5 • SIGN(5.UMC) EF(J) * 5 • SIGN(5.UPC)		J * 2 S(J,K,N) + S(J,K,N) - 5*SMU*(-Z(J-1) +2 *Z(J) -Z(J+1)/P(J,K) J * JH S[J,K,N] * S(J,K,N) - 5*SMU*(-Z(J-1) +2 *Z(J) -Z(J+1)/P(J,K)	00 42 J*3, JMM EP = 1 - EB(J) - EF(J) EH = 1 - EB(J-1) - EF(J) S(J,K,N) = S(J,K,N) - SMU*(EP?Z(J*2) - (3 *EP + EM)*Z(J+1) + 1 3 *(EP +EM)*Z(J) -(EP +3 *EM)*Z(J-1) + EM*Z(J-2)) /P(J,K) 42 CONTINUE	40 CONTINUE C ETA DIRECTION SMOOTHING DO 50 J=2.JH DO 51 K=1.KHAX 51 ZIKI * PLJ.K) DO 52 N=1.4 K * KM K * KM S(J.K.N) * S(J.K.N) - SHU* 5*(-Z(K-1)*Q(J,K-1.N) *2 *Z(K)*Q(J,K.N)
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SUBROUTINE SHOOTH	OTH	92/92	76/76 OPT+2 TRACE	RACE		Ē	FTN 4 6-460	ō	08/60/	01/03/80 11 58 39	PAGE	~
	1 - ZIK	(-1)•0()	K.I.N.	/ZIK)	1 - 21K+11+0(J,K+1,N1)/21K)				SHOOTH	25		
	× 2								SHOOTH	53		
	SCJK	N . S.	, (N.X.)	SMU. 5.1	-Z(K-11.9(J)	K-1.X	-2 •Z(K) •Q(J.K.R.	SHOOTH	25		
	1 - Z(K	(11100)	Îz X	/2(K)					SMOOTH	55		
	00 52	K.3 KHM							SHOOTH	፠		
S.	2 S() X	N . S.	- IN X	SHU*(Z1)	(-2) •Q(J,K-2)	1) Z · (N	(-2) +Q(J, K-2	ź	SHOOTH	57		
	9	Z(K) •00	2 ×	4 *! ZIK	11.0(J.K-1.N	1) •2(K	11:0() K-1	Ē	SECOTA	87		
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AXXX Prop		======================================	ಪ್ತ ಜ≈ಜಜ್ಜ	RET NET TREE						
6ETA+0 NF5G-300 IFINIHE GE NFSG-10-161 IFIJ LT 1018ETA+ 1		SECRETARY OF JIST AND JULE JASTIJA TIJA TIJA TIJA TIJA TIJA TIJA TIJA	0(J,K, I) = 0(J,Z, I)+P(J,Z)/P(J, I) 0(J,K,Z) = 0(J,K,Z)+Q(J,K,I)/PHO 0(J,K,Z) = 0(J,K,Z)+O(J,K,I)/PHO 0(J,K,Z)+FI/GAMI+O 5+:Q(J,K,Z)+*2+Q(J,K,Z)+*21/Q(J,K,I) 31 COMTINE	73 CF 47 INUE C 65 CONTINUE F5 THIS SECTION FOR BOOT • RAMP WALLS	KWHAX DQ 4Q J-J1 J3 RHQ-Q1J,K, 11-P1J,K) UU-(XYIJ,K, 11-Q1J,K, 21-XYIJ,K,21-Q1J,K,21)/Q1J,K,11-X1T(J,K) UXI+Q 5-(Q1J-1,K,21/Q1J-1,K,11-Q1J-1,K,21/Q1J-1,K,11) VXI+Q 5-(Q1J-1,K,31/Q1J-1,K,11-Q1J-1,K,31/Q1J-1,K,11)	IF(J NE J3)GO TO 45 UXI+0 5+(3 +Q(J),K,2)/Q(J),K,11+4 +Q(J-1,K,2)/Q(J-1,K,1)+Q(J-2,K,2)/ +Q(J-2,K,1) +Q(J-2,K,1) -VXI+0 5+(3 +Q(J),K,3)/Q(J,K,1)+4 +Q(J-1,K,3)/Q(J-1,K,1)+Q(J-2,K,3)/ +Q(J-1,K,3)/Q(J,K,1)+4 +Q(J-1,K,3)/Q(J-1,K,1)+Q(J-2,K,3)/ +Q(J-1,K,3)/Q(J,K,1)+4 +Q(J-1,K,3)/Q(J-1,K,1)+Q(J-2,K,3)/	45 CONTINUE FF-R-40-UU-(XYLJ.K.3)-UXL-XYLJ.K.4)-VXLI-R-40-(ETTLJ.KI-DETASILJ)) */OT C************************************	AX11(U.U.K.27(U.U.K.3) AX2-(U.U.K.3)/QU.J.K.11)*XYU.J.K.41 AX3-AX1-AX2 AX4-RHO+(U.J.K.3)/QU.J.K.11)/YU.J.K) FF-FF-AX3-AX4-JAX1 DETAS1(J)*ETT(J.K)	C2*XY(J,K, 31*XY(J,K, 71*XY(J,K, 41) C2*XY(J,K, 31*2-XY(J,K, 41**2 P2*GAM1*(G,J, XM, 41**0 5*(G,J, XM, 21**2-Q,J, NM, 31**2)/G(J, XM, 11) P3*GAM1*(G,J, XM, 41**0 5*(G,J, XM, 21**2-Q,J, XM, 31**2)/G(J, XM, 11) F3*GAM1*(G,J, XM, 41**0 5*(G,J, XM, 21**2-Q,J, XM, 31**2)/G(J, XM, 11) F(J)**FF*C2*(-(1)*F0%01*P2*P(J, XM)**0 5*F0S0*P3*P(J, XM)**1)	A(J):- 5*C1 B(J):- 11 - 0 5*F0S0)*C2 C(J):0 5*C1 40 COXTINE JJJJ-1 PBC-CAH+(0(J):K,4)-0 5*(Q(JJ,K,2)**2*Q(JJ,K,3)**2!/Q(JJ,K,1)) F(J):+F(J):+F(J):+PBC*P(JJ,K)
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01/09/80 11.58.39	N KEEDT N KEEDT	N R R R R R R R R R R R R R R R R R R R	PEUXY PEUXY PEUXY PEEEE
FTN 4.6+460	^• (d	K)) 2)**2*q(J,K,3)**2}/Q(J,K,1) *BETA1*Q(J,K,1)*(1 -BETA1)	FV(3): Q(J,K,2):QS • R1.PP FV(3): Q(J,K,3):QS • R2.PP FV(4) • QS•(Q(J,K,4) • PP) - PP•RO END
76/76 OPT:2 TRACE	CONSTRUCT THE H-VECTOR FAX:(1)+q(J,K,1)*V/P(J,K) FAX:(2)=f(J,K,1)*V*U/P(J,K) FAX:(3)=fAX:(1)*V FAX:(4)+((Q(J,K,4)/P(J,K))+PP)*V	DO 46 N*1,4 CAXIN1=FAXI(N)/(Y(J,K)*P(J,K)) CONTINUE Q(J,K,A)*PP/GAMI+O 5*(Q(J,K,Z)** Q(J,K,A)*PP/GAMI+O 5*(Q(J,K,Z)**	Set Q(J,K,4) + PP)
	CONSTRUCT FAX: (1) *Q: FAX: (2) *Q: FAX: (3) = F/FAX: (4) = (4)	00 46 N*1,4 FAXI(N) =FAXI(N) 46 CONTINUE Q(J,K,4) =PP/CAN Q(J,K,1) = (Q(J,F)	FV(2) FV(3) PO(3)
SUBROUTINE FLUXVE	ა %	65	70

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AMATRX BASE BASE	BASE BASE	VARS	VARS		AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AMATRX	AHATRX	AMATRX	AHATRX	AMATRX
SUBBOUTINE AHATRXIA, J.K.RI.R2) COMMON/BASE/NMAX, JHAX, KHAX, JH. KM.DT.FSMACH.EPS.GAMMA.GAMI.SMU.HD. 1 FV(4), FD(4), RE.P1, Z(80), NP.METH, ALPMA.INVIS, IPLOT.RESID	2. CNPR.IREGO.ISTORE.NF.NB.JTAILF.JTAILZ.IOSCIL.XOSCIL.IUPUND. 3. LAMIN.SMUIM.YARA.YARB.YARC	COMMON/VARS/ Q(78,36,4),XY(78,36,4),P(78,36) COMMON/LARGE/X(78,36),Y(78,36),S(78,36,4),XIT(78,36),ETT(78,36)	LEVEL 2, X, Y, S, XIT, ETT	DIMENSION AV. (4)	CTILL SOBROOTINE CALCOLAIES FRE JACOBIAN NAINITES USED INE EINEARIEA CAMMI - CAMMA -1	BB - 1 0 1 1 1	U = Q(J,K,2)=RR	V = Q(J, K, 3)=RR	V*V • U*U * TU	CI * GANI *UI* 5	<u>.</u>	=	₹.	۳ آھ	0 *	* (-U*U •C1) •R1 -U	•	A(2,3) * - GAHI+V+R1 · U+R2	-		A(3,2) . V=R1 - GAMI=U=R2	A(3,3) * U*R1 +(3 -GAMA)*V*R2	A(3,4) * GAM!*R2	·		7 CS		A(4.4) = GAMHA-QS	RE I URN END
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SUBBOUTINE VISHATIJ)
COMMON/BASEKNHAX, JHAX, KHAX, JH, KH, DT, FSHACH, EPS, GAMMA, GAMI, SHU, HD, OTHION/BASEKNHAX, JHAX, KHAX, JH, KH, DT, FSHACH, EPS, GAMMA, GAMI, SHU, HD, OTHION, SHU, HEGO, ISTORE, INF, NB, JTA, HLI, JTAILZ, IOSCIL, XOSCIL, IUPMND 3, LAMIN, SHUIH, VARA, VARB, VARC
COMMON/VARS/ Q1/8, 36, 41, XT(78, 36, 41, P1/8, 36)
COMMON/LARGEX/XT(78, 36, 1, XT(78, 36, 41, XT(78, 36), ETT(78, 36)
LEVEL 2, X, Y, S, XT E, ETT
COMMON/BRID/ A180, 4, 41, B180, 4, 41, C180, 4, 41, D180, 4, 41, DU180, 4, 41,
                                                                                                                          F (80.4)
COMMON. VISC. U180), V180), C1180), C2180), C3180), C4180), TC180)
COMMON. VISC. TURNU(78,36), SNOR(80), DELST(80), TH0(80), TH1(80)
COMMON. VINHU. FHU(80)
DIMENSION RR(80)
OF THE UNEGRATION PROCESS
DATA PR. PRIR, FRIX, 72, 8,1 3333337
CALL MUKIN(1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 • CC2*V(KR)) *RR(KR)
• CC2*V(K))*RR(K)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       DIK, 2, 3) * CC2*RRIKR)

DUIK, 2, 3) * CC2*RRIK)

DUIK, 2, 4) * 0

DUIK, 2, 4) * 0

DUIK, 2, 4) * 0

DUIK, 2, 1) * 0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      - ( D(K)**2 + V(K)**2)
                                                                                                                                                                                                                                                                  HRE * HD/RE

GPR * GAMMA/PR

DO 10 K*1, KMAX

R1 * 1 /QLJ,K,11

EXS * XYLJ,K,31**2

EYS * XYLJ,K,31**2

EYY * XYLJ,K,31**2

TURN * TURHUCJ,K,

VNU * FMULK) * TURH

GKAP * FMULK) * PRTR*TURH

GKAP * FMULK) * PRTR*TURH
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 C2(K) * VNUJAC*EXY
C3(K) * VNUJAC*EXS * FRT*EYS)
C4(K) * GPR*DJAC*( EXS * EYS)*GKAP
RR(K) * R1
U(K) * R1*Q(J, K, 2)
V(K) * R1*Q(J, K, 3)
TC(K) * Q(J, K, 4)*R1 - ( U(K)**2 * VIK
                                                                                                                                                                                                                                                                                                                                                                                                                                           CICKI = VNUJAC*( FRT*EXS . EYS!
                                                                                                                                                                                                                                                                                                                                                                                                                                                                   CITKI . VNUJAC . FRT . EXS . EYS!
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 CC1 = C1(KR) - C1(K)
CC2 = C2(KR) - C2(K)
CC3 = C3(KR) - C3(K)
CC4 = C4(KR) - C4(K)
D(K, 2, 1) = - ( CC1+U(R)
DU(K, 2, 1) = - ( CC1+U(R)
                                                                                                                                                                                                                                                                                                                                                                                                                            VNUJAC * VNU*DJAC
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            DO 20 K*2.KMAX
KR * K -1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    9
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	SUBROUTINE SHCKOP	нскор	76/76	OPT=2 TRACE	TRACE	FTN 4	FTN 4.6-460	01/09/80	01/09/80 11.58.39	PAGE
_		SUBA	SUBROUTINE SHCKOP(1A, 18)	CKOP(1A	(8)			SHCKOP	(V) (
	U			EBIOUR	. 57 (00)			SHCKOP	? ₹ 1	
u,		ans :	SONIC FRE	E STREA	SUBSONIC FREE STREAM ASSUMED			SHCKOP	ကဏ	
	ى	200 100 100	UST SHOCK 0 I*IA.18	POINT	ADJUST SHOCK POINT OPERATORS DO 10 1×18.18			SHCKOP	~ œ	
		= .	58(1) * E8(1)* (* 1A + 18 -		=			SHCKOP	<u> </u>	
2		10 EF (M) * EF(M)	•EF (M-1	EF(M) . EF(M).EF(M-1)			SHCKOP	=	
	U _.	E G	TURN OFF MOS Fig = 0	T EPS F	LAG SAVE JUST BEFORE SHOC	×		SHCKOP	<u> </u>	
		8	30 20 1-1A 1B					SHCKOP	<u>-</u>	
5		,	J * 14+18 -1 (F(EB(J)) 22 22 21	22 21				SHCKOP	តិ ក	
		21 IFLG	IFLG . IFLG .					SHCKOP	2	
		.F.	IF IFLG GT 3	1 58(3)	0 + (?)			SHCKOP	82	
		≓ 3	GO TO 20					SHCKOP	6	
		22 IFLG : 0	•					SHCKOP	8	
ଷ	_	20 CONTINUE	INUE					SHCKOP	12	
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		2						SHCKOP	23	

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                           FTN 4.6-460
                         SUBROUTINE TRIBIA, B. C. X, F. ML, NU)
DIMENSION A(2), B(2), C(2), X(2), F(2)
C****INVERTS TRID AGONAL HATRICES
TRID, CINL, J/BINL,
NLP1 * NL * 1
DO 1 J*NLP1, NU
Z*1 / (B(J)*F(J)* (J)*I)
X (J)*(F(J)* A(J)*F(J-1))*Z

# F(J)*(F(J)* A(J)*F(J-1))*Z

# F(J)*(F(J)* A(J)*F(J-1))*Z

# NUSPNL*-JI
Z* F(J)*F(J)* X(J)*F(J-1)

RETURN
END
76/76 OPT+2 TRACE
SUBROUTINE TRIB
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01/09/80	RUTUR RUTUR Settur	A RUTUM RUTUM RUTUM RUTUM RUTUM	# # # # # # # # # # # # # # # # # # #	25555 25555 25555 25555 25555 25555 25555 25555 25555 25555 255 2555 255	25.25.25.25.25.25.25.25.25.25.25.25.25.2	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	25.55 25.55
SUBROUTINE MUTUR 76/76 OPT+2 TRACE FTN 4 6-460	C COMPUTE NAMER EDOY VISCOSITY DO 30 K 1, KEDGE	์ ส	C COAD VISCOSITY COEFFS INTO ARRAY, USE INNER VALUE UNTIL C HATCH POINT IS REACHED A 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	K * K * 1 1F (K GT * KEDGE) GO TO 10 1F (TH1 k) LE THO(K!) GO TO 40 41 TURHULL K! * THO(K!) K * K * 1	IF I K LE KEDGEI GO 10 41 10 CONTINUE C REARRANGE TURHUIK! SUCH THAT WHEN AVERAGED AT K AND K-1 C THE CORRECT HIDNAY YALUE WILL BE OBSTAINED	SHP * TURHULJ. I) DO 60 K * 2. KHAX TURKS * TURHULJ.K1 TURHULJ.K1 * 2. O*SHP - TURHULJ.K-1) 60 SHP * TURHS.	80 CONTINUE RETURN END
v	= 15	8	<u>5</u>	8	85.	140	145

APPENDIX B

SOURCE LISTING OF THE GRID GENERATION PROGRAM

01/10/80 14 12 48		HANN HANN HANN HANN HANN HANN HANN HANN		178 178	MAIN 16 MAIN 17 MAIN 18 MAIN 19	MAIN 22	178 178	178 178		INCET78 0 INCET78 9 HAIN 37 HAIN 38		178 178 178	MAIN 47		77 IN 54 IN 15 IS
1/10	X Ž Ž	îîîîîî	ÈÈÌ	X X Z Z Z		Èži	££±£	-23-33	£ 2 :		£ £ 5	* * * * *	ÊŽÎ	řřž	ê£44
FTN 4 6-460	PROGRAM MAINCINPUT, TAPES-INPUT, OUTPUT, TAPEG.OUTPUT, TAPE48, TAPE81 LOGICAL UNIT NUMBERS USED IN THIS PROGRAM	READ IMPUT DATA CARDS WRITE PRINTER OUTPUT UNFORMATTED WRITE OF FINAL SOLUTION GRID SC4020 PLOTTER DATA		DIMENSION XB(140), YB(140), X(1140,80), Y(1140,80) DIMENSION LINE(8) DIMENSION XP(140,80), YP(140,80) DIMENSION NP(140)	GRIDS ARE PRESENTLY LIMITED BY DIMENSION SIZE TO 140 POINTS IN XI DIRECTION THESE DIMENSION SIZES ARE FOUND IN SUBROUTINES INNER, OUTER, RELAX. CLUSTR, EPSIL, AND PLANT AS WELL AS HERE IN THE MAIN PROGRAM		READ IN PARAMETERS READIS, 101) JWAKE, KMAX, MLYIT IDSPLY READIS, 1021XGHX, XGMN, YMAX, YMIN, XNOSE, XTAIL, XRAMP READIS, 1021, 071	PG_ETACD_BETA READIN	(X. HAXIT, XGHX, XGHN, YHAX, YMIN, XNOSE, XTAIL,	XHAMP WRITE(6,1131 DY1,XORG,YORG,ETACD,BETA,OHEGA.DY2 WRITE(6,109) LIME ETAC:ETACO:P1/180	Заун	=	(N_XB(N)_YB(N)_N*1_NBOD)	DISTRIBUTE POINTS ON INNER AND REAR BOUNDARIES L'INNERINBOD, JWAKE, KMAX XB, YB, XNOSE XTAIL, YGMX, YMAX, YMIN, TI, JMAX, X, YI	DISTRIBUTE POINTS ON BOTTOM-FPONT-TOP BOUNDARY CALL OUTERIXCMX,XGMN,TMAX TMIN.XORG,YGRG,ETAC,BETA, JMAX,KMAX,X,Y, «XRAMP)
OPT.2 TRACE	CINPUT. TA	D INPUT D TE PRINTE DRMATTED D20 PLOTTI	ITITLE181	(140), YB(NE(8) (140,80), (140)	PRESENTL ECTION AM SIZES AR USTR, EPS RAH	15926547	ARAMETERS JYAKE, KHA GHX, XGMN, DY?	XORG, YOR OMEGA DY2 Q LICALL TITLE	JWAKE KHA	DY 1, XORG ITITLE LINE I/180	IRF1OL SH	B(N) .YB(N	(N XBIN	E POINTS - BOD, JWAKE . Y J	E POINTS OMX, XGHN,
76/76	ROGRAM MAIN LOGICAL UI	5	COMMON/TCOM/ITITLE(8)	IMENSION XB IMENSION LI IMENSION XP IMENSION NP	GRIDS ARE PRECTOR NOT BELLAX. CLUSTE HALLS PROCERAM	DATA PIZ3 1415926547	READ IN P EAD(5,101) EAD(5,1021X EAD(5,102)	READ(5, 102) XORG READ(5, 102) CMEG READ(5, 102) DY2 1F(105PLY EQ 11) READ(5, 100) ITILE DEFACE OCC	RITE(6,112)	HARP RITE(6, 1131 RITE(6, 137) RITE(6, 1091 TAC:ETACO*P	READ IN AIRFIOL	DD 2 N=1, NBOD READIS, 1021XB(N), YB(N) CONTINE	WR1TE16.1041	DISTRIBUTE P CALL INNERINBOD DYI, JHAX, X.YI	DISTRIBUTA ALL OUTERIX
PROGRAM MAIN		عورون			,0000u		. J	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	ž 5€: U	¥	ധ	~ ~			9.≵
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14.12.48	8 5 5 8 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8				177 1867 1867 1867	35 G G	5 4 8855	~%% % %%	38888	88888 88888	88884444 8880-4884
01/10/80	ZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZ	E E E E E E E E E E E E E E E E E E E	ZZZZZ K Z Z Z Z Z Z Z Z Z Z Z	HAIN HAIN HAIN	MAIN INLET78 MAIN MAIN	MAIN HAIN	MAIN MAIN MAIN MAIN T INLET78	INLET78 INLET78 INLET78 INLET78 INLET78 INLET78	INLET78 INLET78 INLET78 INLET78 INLET78	INLET78 INLET78 INLET78 INLET78 INLET78	INCET78 INCET78 INCET78 INCET78 INCET78 INCET78 INCET78 INCET78 INCET78
r IN 4 6+460	C FILL-IN BETWEEN ETA-MAX AND ETA-MIN BOUNDARIES. 34 JMM = JMAX -1 KMM = KMAX -1 RKMM = KMAX -1		DO 13 K=2.KMM X(J,K) = X(J,I) + (K-!)*DELX 13 Y(J,K) = Y(J,I) + (K-!)*DELY C PLOT IN) TIAL CONDITIONS	FFIDSPLY EQ. IICALL PLANTIUMAX,KHAX,X,Y,XGMX,XGHN,YMAX,YHINI C GENERATE UN-CLUSTERED GRID CALL RELAXIUMAX,KMAX,X,Y,OMEGA,MAXITI	-		C WRITE FINAL SOLUTION MRITE(B) (KKIJ,KJ,J#1,JMAX), K*1,KMAXI,(KTJ,K),J#1,JMAX1,K*1,KMAX) CDISPLAY INNER AND OUTER BOUNDARIES USING J MULLEN'S PRINTER PLOT 10PT*3	LENG= 100 LENG= 100 NDP= 140 NC=4 NP 1 1 = JMAX	NP(3)=UMAX NP(4)=UMAX DO 40 J=1 JMAX XP(J, 1)= XX(L, 1) YP(J, 1)= X(L, 1)	XP(J, 2) *X(J, XNAX) XP(J, 2) *Y(J, XNAX) XP(J, 3) *X(J, 5) YP(J, 3) *X(J, XNAX) XP(J, 4) *X(J, XNAX)	YP(J,4)=Y(J,KHH) 40 CONTINUE CALL PLOTAZIKP,YP,10PT,NP.NDP,NC,LW1D,LENG) GO TO 555 C DISPLAY ALL GRID LINES NC.JMAX/5.1 N.O.
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SUBROUTINE RELAX	NE RELY	76/76	OPT*2 TRACE	FTN 4.6+460	01/10/80 14.12.48	14, 12, 48	PAGE
09	75	WRITE(6, 117) WRITE(6, 116) WRITE(6, 117)	WRITE(6,117) (X(J.K),K*1,KMAX) WRITE(6,116)J WRITE(6,117) (Y(J.K),K*1,KMAX)		RELAX	609 609	
		RETURN			RELAX RELAX	633 633 633	
65		FORMAT(20H SUM 1 7H AFTER ,15, FORMAT(/31H X	OF RESIDUALS = F20.10, 12H TERATIONS.) S FOR CONSTANT XI LINF AT 1: 16	Ī.	RELAX RELAX RELAX	65 66 67	
	222	FORMAT(/31H Y FORMAT(10E13 6	FORMATIVELY S FOR CONSTANT XI LINE AT J: 15) FORMATIVELS 6) FORMATIVELS AT TANABONE COLVED DEFORE FINAL CHIEFDING 1	5)	RELAX	888 200 200 200 200 200 200 200 200 200	
20		END	ובע ומסובססוג-ססרינה, פברסה רוב	יאר כרסטובעוואפין	RELAX	22	

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SUBROUTINE TRIB	NE TRIB	76/76 06	OPT*2 TRACE	FTN 4.6+430	01/10/80 14.12.48	14.12.48	PAGE
-	·	SUBROUTINE TRIB DIMENSION A(2).	SUBROUTINE TRIBIA, B.C.X.F.NL.NU) DIMENSION A(2), B(2), C(2), X(2), F(2)		8187 8181 8181	W €	
വ	ىەنەد	THIS SUBROUT EQUATIONS.	THIS SUBROUTINE SOLVES A TRI-DIAGONAL SYSTEM OF LINEAR EQUATIONS.	1 OF LINEAR	<u> </u>	1000	
		X(NL)=C(NL)/B(NL) F(NL)=F(NL)/B(NL)	55		17. 17. 18. 18. 18. 18. 18. 18. 18. 18. 18. 18	. 	
0		NLP1 = NL +1 D0 1 J=NLP1 NU Z=1 /(B(J)-A(J)*X(J-1)	.X(J-11)		2 E E E	2=25	
	-	X(J)=C(J)*Z F(J)=(F(J)-A(J)*F(J-1))*Z NIPN=NJ+N	*F(J-1))*Z		7.7.7. 7.7.7.7. 8.8.8.8.8.8.8.8.8.8.8.8.	<u>5 4 f</u>	
<u> </u>		DO 2 JI=NLP1 NU J=NUPNL - J1			17.18 17.18	16 17	
	CV	F(J)=F(J)-X(J)*F(J+) RETURN END	٦(١٠٠) ٩		TR 18	860	

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SUBROUT	SUBROUTINE PLOT	76/76 OPT*2 TRACE	0PT±2	TRACE	NET	FTN 4.6+460	01/10/80 14.12.48	14.12.48	PAGE
-	¢	SUBROUTINE PLOT(X, Y, NBR, NSYM)	.OT(X,Y	.NBR.NSYM)			PLOT	W	
	JUU	THIS SUBRO	UTINE 1020 PL	IS ONE OF THO	THIS SUBROUTINE IS ONE OF THOSE THAT PLOTS GRIDS ON THE SC4020 PLOTTER.	SC	252	ລ∡ເບ (
្		DIMENSION XI	1).Y(1)	.MARKPT(5)			74	ονα	
	ပ	SYMBOLS ARE.	ORO O	SYMBOLS ARE, IN ORDER: - X O . JE (NSYM OF B) CO TO 100	20 10 100		201	ທີ	
9		J= {ABS(NBR)-1					P_01	2=2	
	011	CONTINUE	EV 1 1X	V(X(L)), LYV(CALL LINEVE XV(X(1)), TYV(Y(1)), TXV(X(1+1)), TYV(Y(1+1)) NUF	1, 1YV(Y(1+1)) 1	250	<u> </u>	
15	8	RETURN CALL APLOTY ()	IBR.×.Υ	RETURN CALL APLOTV(NBR, X, Y, 1, 1, 1, MARKPT(NSYM))	(NSYM))		P. 01	:20	
		RETURN END					P.01	7 81	

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16. Abstract							
The use of a comp	uter code f	for the calcu	lation of :	2-D inlet			
flow fields in a super	sonic free	stream and a	nonorthogo	onal mesh-			
generation code are il	lustrated b	y specific e	xamples.	Input,			
output and program ope	ration and	use are give	n and expla	ained for			
the case of supercriti	cal inlet o	peration at	a subdesign	n Mach			
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inlet. Source listing	s of the co	mputer codes	are also	provided.			
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calculation method inlets							
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